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#### Not for citation

#### Measuring U.S. Agriculture Productivity: Primal vs. Dual Approaches

#### Introduction

There is an ongoing discussion about whether U.S. agricultural productivity growth has recently slowed down. Differing views are supported by productivity estimates obtained from different datasets and econometric approaches, as well as primal versus dual representations of the underlying technology. This study contributes to the ongoing discussion by shedding light on how the choice of dual versus primal approaches, and the imposition of certain restrictions in estimation, affect the estimated productivity trends when the same dataset is used across models.

Plastina and Lence (2015) were the first to assess the effects of jointly imposing monotonicity and concavity conditions derived from economic theory on an aggregate representation of U.S. agricultural technology in the primal space. Previous applied production studies using flexible functional forms fell short of imposing both monotonicity and curvature conditions in estimation, and instead reported the proportion of the sample for which those conditions did not hold, warning readers about potential unknown biases introduced by those observations that did not conform to production theory.

Plastina and Lence (2015) found that not only the shapes but also the locations of the probability density functions (pdfs) of the parameter estimates were significantly affected by the imposition of those theoretical restrictions. As a result, output elasticities and multifactor productivity estimates also differed substantially between restricted and unrestricted models. Finally, for the estimates recovered from the dataset (Ball et al. 2004) to conform to production theory, both concavity and monotonicity at each data point had to be imposed in estimation.

The present study extends the analysis by Plastina and Lence (2015) into the dual space, and provides an encompassing comparison of productivity measures and technological characterizations of U.S. agriculture not only across restricted and unrestricted models, but also across primal and dual approaches.

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The goals of the present study are twofold. The first goal is to analyze the effects on the estimated parameter pdfs caused by the restrictions stemming from production theory, for the case of a variable cost function representation of U.S. agricultural technology. The second goal is to evaluate the impact on multifactor productivity estimates of using dual versus primal representations of the agricultural technology.

#### Model

Since technology constrains the optimizing behavior of economic agents, one should be able to use an accurate representation of optimizing behavior to study the technology (Chambers 1996, p. 49). Assuming (1) the existence of a production function, y = f(X), that shows the maximum output, y, attainable from an arbitrary vector  $X \equiv [x_1, \dots, x_n]$  comprising the levels of n inputs; (2) which satisfies monotonicity and weak essentiality in X; and (3) that the input requirement set,  $B(y) = \{X: f(X) \ge y\}$ , is closed, non-empty and convex; then a well-defined variable cost function C = C(W, y) exists which exhibits the following characteristics (Chambers 1996):<sup>1</sup>

- 1. Non-negativity,  $C = C(W, y) \ge 0$ .
- Non-decreasing in input prices, W ≡ [w<sub>1</sub>, ..., w<sub>n</sub>]. If any input price increases, cost must not decrease, ∇<sub>W</sub>C(W, y) ≥ 0.
- 3. Concave and continuous in *W*. Concavity is a direct result of the cost minimizing behavior (input price changes generate opposite direction changes in input utilization, ∇*W* · ∇*X* ≤ 0), and it does not impose any condition on the underlying technology. Assuming that the cost function is twice differentiable with respect to input prices, concavity requires the matrix of second order derivatives of the cost function with respect to input prices, *H* ≡ ∇<sup>2</sup><sub>W</sub>C(*W*, *y*), to be negative semidefinite.

<sup>&</sup>lt;sup>1</sup> If the input requirement set is convex and monotone, then the technology represented by the cost function will be identical to the true input requirement set. If the true input requirement set is non-convex or non-monotone, the derived input requirement set will be a convex and monotone version of the true set and, most importantly, the derived technology will have the same cost function as the true one (Varian 1992, Ch. 6).

- 4. Positively linearly homogeneous in W,  $\lambda C(W, y) = C(\lambda W, y)$  for any  $\lambda > 0$ . This property implies that only relative prices matter to economically optimizing agents.
- 5. Non-decreasing in *y*.

The econometric estimation of the cost function requires selecting a specific functional form for the latter. In the present study, the following generalized quadratic cost function is used to represent the optimizing behavior:

(1) 
$$C(W, y, t) = \gamma_0 + \sum_{i=1}^n \gamma_i w_i + \gamma_t t + \gamma_y y + \frac{1}{2} \sum_{i=1}^n \sum_{j=1}^n \gamma_{ij} w_i w_j + \sum_{i=1}^n \gamma_{ti} w_i t + \sum_{i=1}^n \gamma_{yi} w_i y + \gamma_{yt} y t + \frac{1}{2} \gamma_{tt} t^2 + \frac{1}{2} \gamma_{yy} y^2,$$

where  $\gamma_{ij} = \gamma_{ji}$  by Young's theorem. To allow for changes in the shape of the cost function through time, expression (1) incorporates a time trend, *t*, that enters the function in levels, interacted with inputs, and squared.

There are good reasons for employing the generalized quadratic function (1) for estimation purposes. Most importantly, it is a flexible functional form, both in the sense of being a second-order Taylor series (numerical) approximation to an arbitrary non-linear function, and in the sense of being a second-order differential approximation (with its function value, gradient, and Hessian equal to the corresponding magnitudes for any arbitrary general non-linear function evaluated at a certain level of its underlying arguments). In addition, the generalized quadratic allows for imposition concavity globally<sup>2</sup> in estimation, and is self-dual.<sup>3</sup>

In terms of the generalized quadratic, the aforementioned properties of the cost function can be expressed as a set of parametric restrictions, as follows. First, non-negativity requires that

(2) 
$$C(W, y, t) = \gamma_0 + \sum_{i=1}^n \gamma_i w_i + \gamma_t t + \gamma_y y + \frac{1}{2} \sum_{i=1}^n \sum_{j=1}^n \gamma_{ij} w_i w_j + \sum_{i=1}^n \gamma_{ti} w_i t + \sum_{i=1}^n \gamma_{yi} w_i y + \gamma_{yt} y t + \frac{1}{2} \gamma_{tt} t^2 + \frac{1}{2} \gamma_{yy} y^2 \ge 0.$$

 $<sup>^{2}</sup>$  Alternative flexible functional forms, such as the translog, do not allow for the global imposition of concavity in estimation. Using filters, concavity can only be imposed locally in estimation (for a particular point in time, or at the means of the data).

<sup>&</sup>lt;sup>3</sup> Self-duality will prove useful to expand the present analysis to include profit functions in future research.

Second, a cost function non-decreasing in W requires that

(3) 
$$\frac{\partial c(W,y,t)}{\partial w_i} = x_i(W,y,t) = \gamma_i + \sum_{j=1}^n \gamma_{ij} w_j + \gamma_{ti} t + \gamma_{yi} y \ge 0,$$

where the first equality holds by Sheppard's lemma, and  $x_i(W, y)$  is the unique, cost minimizing demand for input  $x_i$ . Third, concavity requires the Hessian,

(4) 
$$H \equiv \nabla_W^2 C(W, y), = \begin{bmatrix} \gamma_{11} & \cdots & \gamma_{1n} \\ \vdots & \ddots & \vdots \\ \gamma_{1n} & \cdots & \gamma_{nn} \end{bmatrix},$$

to be negative semidefinite. Fourth, homogeneity of degree 1 in W can be imposed in estimation through the following set of n + 1 restrictions:

(5a) 
$$\sum_{j=1}^{n} \gamma_{ij} w_j = 0$$
, for  $i = 1, ..., n$ 

(5b) 
$$\gamma_0 + \gamma_t t + \gamma_y y + \gamma_{yt} y t + \frac{1}{2} \gamma_{tt} t^2 + \frac{1}{2} \gamma_{yy} y^2 = 0.$$

Finally, the cost function is non-decreasing in *y* if the marginal cost is non-negative:

(6) 
$$\frac{\partial C(W,y,t)}{\partial y} = \gamma_y + \sum_{i=1}^n \gamma_{yi} w_i + \gamma_{yt} t + \gamma_{yy} y \ge 0.$$

To analyze the effects of imposing cost function restrictions in the estimation of equation (1), we consider the following models:

- Model 1: Unrestricted estimation
- Model 2: Non-negativity constrains i.e. conditions (2), (3), and (6) imposed in estimation at data means.
- Model 3: Non-negativity constrains imposed at all data points in estimation.
- Model 4: Concavity imposed in estimation.
- Model 5: Concavity and non-negativity constrains imposed in estimation at data means.

- Model 6: Concavity and non-negativity constrains imposed at all data points in estimation.
- Model 7: Linear homogeneity, i.e. equations (5a) and (5b), imposed in estimation at data means.
- Model 8: Concavity and linear homogeneity imposed in estimation at data means.
- Model 9: Concavity, non-negativity constrains, and linear homogeneity imposed in estimation at data means.
- Model 10: Concavity, non-negativity constrains at all data points, and linear homogeneity at data means imposed in estimation.

More specifically, under non-negativity constrains at data means, conditions (2), (3), and (6) are satisfied when evaluated at the sample averages of the input prices and output levels, and the time variable. Non-negativity constrains at all data points is a far more stringent constraint, as it involves satisfying restrictions (2), (3), and (6) at each of the input prices and output levels, and the time values contained in the data set.

For each model, the elasticity of cost with respect to output, and the rate of disembodied technical change are calculated using expressions (7) and (8), respectively:

(7) 
$$\varepsilon_{CY} = \frac{\partial C(W,y,t)}{\partial y} \frac{y}{C(W,y,t)} = \left(\gamma_y + \sum_{i=1}^n \gamma_{yi} w_i + \gamma_{yt} t + \gamma_{yy} y\right) \frac{y}{C(W,y)}$$

(8) 
$$\varepsilon_{Ct} = \frac{\partial C(W,y,t)}{\partial t} \frac{1}{C(W,y,t)} = \left(\gamma_t + \sum_{i=1}^n \gamma_{ti} w_i + \gamma_{yt} y + \gamma_{yt} t\right) \frac{1}{C(W,y)}$$

The elasticity of cost with respect to output is indicative of the returns to scale in production at the cost-minimizing bundle: if  $\varepsilon_{CY} < 1$  production is characterized by increasing returns to scale; and if  $\varepsilon_{CY} > 1$  production is characterized by decreasing returns to scale (Chambers 1988). The rate of disembodied technical change indicates the average percentage decline in costs due to increases in multifactor productivity.

Price elasticities for each variable input and the semi-elasticity of input demand with respect to time are calculated using expressions (9) and (10), respectively:

(9) 
$$\varepsilon_{x_i w_j} = \frac{\partial^2 C(W, y, t)}{\partial w_i \partial w_j} \frac{w_j}{\partial C(W, y, t) / \partial w_i} = \frac{\partial x_i(W, y, t)}{\partial w_j} \frac{w_j}{x_i(W, y, t)} = \frac{\gamma_{ij} w_j}{x_i(W, y, t)}$$

(10) 
$$\varepsilon_{x_i t} = \frac{\partial^2 C(W, y, t)}{\partial w_i \partial t} \frac{1}{\partial C(W, y, t) / \partial w_i} = \frac{\gamma_{ti}}{x_i(W, y, t)}.$$

We first analyze the differences in the estimated elasticities, semi-elasticities, and the rate of technical change across models to examine the implications of imposing cost function restrictions in the estimation of equation (1). Then, we compare the returns to scale and the rate of technical change obtained in this study against similar measures obtained from a generalized quadratic production function fit to the same data set (Plastina and Lence 2015).

#### Data

Models 1 through 6 are estimated by employing the official USDA panel dataset on agricultural production for the United States (USDA 2015, Table 23<sup>4</sup>). The dataset is described in Ball et al. (2004) and its main use is the calculation of TFP as the ratio of an index of output quantities to an index of input quantities. The panel was specifically developed to measure agricultural productivity. Earlier versions of the data were used by Morrison Paul et al. (2001), Huffman et al. (2002), and Wang et al. (2012) to evaluate agricultural productivity by means of a cost function; and by Plastina and Lence (2015) to evaluate productivity in primal space.

The dataset contains one aggregate agricultural output and n = 3 variable inputs (capital, labor, and materials) for each of the S = 48 contiguous states over the period 1960-2004, i.e., T = 45 annual observations. All quantities are measured as transitive implicit Fisher quantity indexes, or "EKS" indexes based on the work of Eltetö and Köves (1964), and Szulc (1964), calculated with price indexes with bases equal to unity in Alabama in 1996. The transitivity of the quantity indexes ensures that indexes are comparable across states and years.

<sup>&</sup>lt;sup>4</sup> The dataset was updated on May 9, 2016, and the aggregate capital variable is no longer reported. Capital is disaggregated into Capital services excluding land and Land service flows in the new dataset.

The output quantity, y, measures the aggregate production of livestock, dairy, poultry, eggs, grains, oilseeds, cotton, tobacco, fruit, vegetables, nuts, and other miscellaneous outputs. Capital,  $K \equiv x_1$ , measures the service flows of real estate, durable equipment, and stocks of inventories. Labor,  $L \equiv x_2$ , measures the quality-adjusted amount of hired and self-employed labor. Materials,  $M \equiv x_3$ , include fertilizers, pesticides, energy and other miscellaneous inputs. Cost,  $C \equiv C(W, y, t)$ , is constructed as the summation of the products of input quantities and input prices. Summary statistics for output and the three inputs are reported in Table 1.

#### **Estimation Methods**

Estimation is conducted by setting up equations (1) and (3) as a seemingly unrelated regressions (SUR) system. The dependent variables in the four SUR equations are cost (corresponding to equation (1)), and capital, labor, and materials (corresponding to equation (3)). The system is estimated by imposing the restrictions in the regression coefficients stated in equations (1) and (3).<sup>5</sup> Because all four dependent variables are highly autocorrelated, the first lag of the corresponding dependent variable was added as an explanatory variable to each of the four equations, and their coefficients denoted by  $\alpha_C$ ,  $\alpha_K$ ,  $\alpha_L$ , and  $\alpha_M$  for cost, capital, labor, and materials, respectively.

The parameters of the SUR model are the 21 regression coefficients included in equations (1)-(3), the four coefficients corresponding to the lagged dependent variables, and the ten parameters involved in the covariance matrix of the regression residuals (consisting of four standard deviations  $\sigma_i$  and six correlation coefficients  $\rho_{ij}$ ). We estimate the model's 35 parameters by employing Bayesian Hamiltonian Monte Carlo (HMC) sampling (Duane et al., 1987; Neal, 1994, 2011). The SUR HMC model is fitted using version 2.9.0 of the RStan program (Stan Development Team, 2015) and version 3.3.0 of the R software (https://www.r-project.org/).

<sup>&</sup>lt;sup>5</sup> For example, the regression coefficient for the cross product of time and wages in the cost equation (1),  $\gamma_{tW_L}$ , is the same as the time coefficient in equation (3) for labor.

Bayesian techniques are quite useful for the present application, because they allow us to impose the desired estimation restrictions in a straightforward manner. Another advantage of the Bayesian approach is that it yields full posterior distributions for the parameters of interest. This feature is particularly useful when researchers try to characterize parameters with skewed posteriors, such as the parameters subject to concavity restrictions. Further, pdfs for the elasticities and the rate of technical change can be computed directly from the estimated pdfs for the underlying parameters, rather than by quadratic approximation (e.g., as in the delta method).

The Bayesian procedure is explained next by focusing on Model 6 (i.e., the most restrictive specification). Models 1 through 5 are estimated using the same method, except for the relaxation of the corresponding parameter constraints. Estimation proceeds by conditioning on the initial set of observations (i.e., the variable values observed at t = 1) (Lancaster 2004, Ch. 9). The priors are half-Cauchy for the standard deviations of the residuals ( $\sigma_i \sim \text{Cauchy}(0, 2.5)$ ) for  $\sigma_i > 0$ , LKJ for the correlation matrix of the residuals (Residual Correlation Matrix ~ LKJcorr(4)), and weakly informative normal for the lagged-dependent variable regression coefficients, as well as for the regression coefficients not included in the Hessian ( $\gamma_i \sim Normal(0, \gamma_i)$ 5)). Since a negative semidefinite Hessian  $H = [\gamma_{w_K w_K}, \gamma_{w_K w_L}, \gamma_{w_K w_L}, \gamma_{w_L w_L}, \gamma_{w_L w_M}; \gamma_{w_L w_L}, \gamma_{w_L w_M}; \gamma_{w_L w_L}, \gamma_{w_L w_M}; \gamma_{w_L w_L}, \gamma_{w_L w_M}; \gamma_{w_L w_L}, \gamma_{w_L w_L}, \gamma_{w_L w_M}; \gamma_{w_L w_L}, \gamma_{w_L$  $\gamma_{w_K w_M}, \gamma_{w_L w_M}, \gamma_{w_M w_M}$ ] implies that the symmetric (3 × 3) matrix  $\Omega = -H$  is positive semidefinite, we compute H by first setting the same priors for  $\Omega$  as for the covariance matrix, and then recovering the Hessian parameters from the relationship  $H \equiv -\Omega$ . That is,  $\Omega = D(3)$ Corr(3) D(3), where D(3) is a  $(3 \times 3)$  diagonal matrix and Corr(3) is a  $(3 \times 3)$  of matrix correlation coefficients, so  $[D(3)]_{ii} \sim \text{Cauchy}(0, 2.5)$  for  $[D(3)]_{ii} > 0$ , and  $\text{Corr}(3) \sim \text{LKJcorr}(4)$ . Finally, to ensure positive costs, capital, labor, materials, and output at all observation points, minimum values of coefficients  $\gamma_0$ ,  $\gamma_{W_K}$ ,  $\gamma_{W_L}$ ,  $\gamma_{W_M}$ , and  $\gamma_Y$  are imposed so as to meet the positivity restrictions.<sup>6</sup>

<sup>&</sup>lt;sup>6</sup> For example, the restriction  $\gamma_y \ge -\min(\gamma_{yt} t + \gamma_{yw_K} w_K + \gamma_{yw_L} w_L + \gamma_{yy} y)$  is imposed to guarantee that condition (6) is met.

#### **Results and Discussion**

Estimation results for Models 1 through 6 for the state of Iowa are reported in Table 2. For each model, this table shows the means of the parameters of interest, as well as their standard deviations, medians, and 95% credible intervals.<sup>7</sup> For example, the unrestricted (i.e., Model 1) mean of parameter  $\gamma_Y$  equals -0.6251, with a standard deviation of 0.5701, a median equal to - 0.6228, and a 95% credible interval ranging from -1.7344 to 0.4542.

It is evident from the figures in Table 2 (compare, e.g., the estimates of parameter  $\gamma_Y$  and the likelihood values across models) that the choice of model has only minor implications for the characterization of the production technology, and therefore for the policy recommendations stemming from it. This finding is in stark contrast to the conclusion in Plastina and Lence (2015) that imposing restrictions stemming from production theory in estimation of a generalized quadratic production function has a substantial effect on the characterization of U.S. agricultural production technology.

The point estimates of the coefficients for the lagged dependent variables range between  $\alpha_c = 0.4831$  for Model 3, and  $\alpha_c = 0.5334$  for Model 4;  $\alpha_K = 0.9079$  for Model 3, and  $\alpha_K = 0.9432$  for Model 4;  $\alpha_L = 0.3419$  for Model 6, and  $\alpha_L = 0.3678$  for Model 2;  $\alpha_M = 0.3770$  for Model 3, and  $\alpha_M = 0.4533$  for Model 4. In all instances, credible intervals are very tight and with lower bounds far from zero, providing a strong indication that adjustments occur over multiple periods. The derived demand for capital exhibits high inertia, but significantly less than 1 for all models but Model 3. The goodness of fit is consistent across Models 1 through 6, indicating that non-negativity and concavity restrictions are not too burdensome to the explanatory power of the model. It must be noted that, in general, the same qualitative results arise from Models 1 through 6.

The elasticity of cost with respect to output is positive and significantly lower than 1 in all models (except Model 4), indicating that agricultural production in Iowa is characterized by

<sup>&</sup>lt;sup>7</sup> Credible intervals are the Bayesian analogs of confidence intervals. The upper and lower bound of the 95% credible intervals reported here are the 2.5% and 97.5% quantiles of the corresponding posterior distributions.

increasing returns to scale in the dual space (Table 3). This is an interesting finding given that Plastina and Lence (2015) report decreasing returns to scale for the U.S. aggregate in primal space across all models (those with concavity<sup>8</sup> imposed in estimation, and those where concavity was not imposed in estimation), using the same database.

The rate of disembodied technical change is significantly different from zero in all models, and the point estimates range between -0.74% for Model 2 and -0.84% for Model 3. Plastina and Lence (2015) report a 1.5% rate of technical change in primal space for Iowa, and 1.45% for the U.S. aggregate for 1960-2004.

As expected, the own-price elasticity of capital is negative and significantly different from zero, ranging from -0.1326 in Model 6 to -0.1512 in Model 1 (Table 4). The price elasticity of capital with respect to labor is negative, but not significantly different from zero in Models 1-6. The price elasticity of capital with respect to materials is positive and significantly different from zero for all models (except Model 4), with a point estimate ranging from 0.0564 in Model 4 to 0.0958 in Model 3.

The own price elasticity of labor is negative and significantly different from zero, ranging from -0.0866 in Model 4 to -0.0612 in Model 3 (Table 5). The price elasticity of labor with respect to capital is negative, but not significantly different from zero in Models 1-6. Similarly, the price elasticity of labor with respect to materials is negative, but not significantly different from zero in Models 1-6.

The own price elasticity of materials is negative and significantly different from zero for Models 4-6, ranging from -0.0859 in Model 4 to -0.0934 in Model 6 (Table 6). For Models 1-3, the point estimates of the own price elasticity of materials have the expected sign, but the 95% confidence intervals include the null value. The price elasticity of materials with respect to capital is positive (ranging from 0.0151 in Model 4 to 0.0258 in Model 3), and significantly different from zero in all Models except for Models 4 and 5. The price elasticity of materials with respect to labor is negative, but not significantly different from zero in Models 1-6.

<sup>&</sup>lt;sup>8</sup> Imposing concavity on the production function rules out increasing returns to scale.

Succinctly, the price elasticities indicate that (1) labor demand is not strongly responsive to capital or material prices; (2) capital and materials are substitutes; and (3) own price effects on input demand dominate cross-price effects.

The semi-elasticities of input demands with respect to time suggest that technical change has not been Hicks-neutral. Instead, technical change been labor-saving ( $\varepsilon_{Lt} < 0$  and significant across models in Table 5), material-saving ( $\varepsilon_{Mt} < 0$  but not significant across models in Table 6), and capital-using ( $\varepsilon_{Kt} > 0$  but not significant across models in Table 4). Plastina and Lence (2015) also report non-Hicks-neutral technical change, although they conclude that over time output has become more responsive to changes in materials and labor, and less responsive to changes in capital.

#### **Concluding Remarks**

The economic theory of producer behavior requires certain conditions to hold in order for a functional form to be representative of a production technology. Agricultural production studies are usually conducted using classical econometric methods that make it difficult, if not impossible, to impose such restrictions in flexible functional forms. Therefore, conditions required by economic theory need not hold in estimation. Using state-level panel data on U.S. agricultural production to fit a generalized quadratic cost function, we estimated six models characterized by different restrictions for Iowa. More specifically, Model 1 is unrestricted, whereas Models 2 through 6 impose respectively the following restrictions in estimation: non-negativity of the cost function at data means, non-negativity of the cost function at all data points, concavity, both concavity and non-negativity of the cost function at all data points.

Each model is estimated using Bayesian methods. A desirable feature of the proposed Bayesian procedure is that it greatly facilitates imposing concavity, non-negativity and homogeneity conditions. In addition, the procedure yields simulated parameter values from their

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posterior pdfs, which can be used to compute simulated pdfs for functions of such parameters, such as price elasticities, elasticities of scale, and technical change.

Contrary to what Plastina and Lence (2015) found in the primal space, imposing restrictions in the cost function does not qualitatively change the characterization of the underlying agricultural technology.

Disembodied technical change generated, on average, cost savings of about 0.8% per year over 1961-2004 in Iowa.

This is an ongoing work and we plan to estimate the model using all 48 states, and expand the analysis to include homogeneity of degree 1 for the cost function (Models 7-10). Finally, the analysis will be completed by comparing estimates of technical change on the dual space with estimates obtained in primal space, using the same database.

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Indexes	Unit	Mean	Median	Standard Deviation	Minimum	Maximum
Cost value	Million \$1996	9,291.1	10,860.5	3,557.2	3,427.4	14,127.6
Capital quantity	Million \$1996	2,353.9	2,257.8	500.5	1,716.6	3,275.4
Labor quantity	Million \$1996	5,127.1	5,309.9	1,544.8	2,541.7	7,918.6
Materials quantity	Million \$1996	6,275	6,202	586	5,518	7,548
Price of Labor	Unitless*	0.641	0.802	0.363	0.148	1.105
Price of Capital	Unitless*	0.547	0.434	0.408	0.129	1.580
Price of Materials	Unitless*	0.894	1.057	0.341	0.359	1.319
Output quantity	Million \$1996	13,034.6	12,866.2	1,828.9	10,138.5	16,362.1

# Table 1. Descriptive statistics, 1961-2004

\*Ratio of prices in each state and year to corresponding price in Alabama in 1996.

Table 2.	Parameter	estimates	for	Models	1	through 6	, ,

Table 2. Farame	ier estimat	es jur Mill	iers i lillo	ugn 0.		
γo	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	3.7747	3.7386	2.1589	3.8845	3.7742	2.1664
Median	3.7587	3.8121	2.2238	3.9196	3.7425	2.2734
Stdev	3.7304	3.7258	2.4089	3.8359	3.6925	2.4022
Lower Bound^	-3.3771	-3.5357	-2.7400	-3.7407	-3.3768	-2.7496
Higher Bound^	10.8817	11.1129	6.7974	11.5088	11.2281	6.7864
$\gamma_t$	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	0.1570	0.1595	0.1211	0.1513	0.1550	0.1154
Median	0.1560	0.1579	0.1174	0.1506	0.1551	0.1121
Stdev	0.1139	0.1127	0.0783	0.1192	0.1127	0.0760
Lower Bound^	-0.0717	-0.0657	-0.0230	-0.0769	-0.0583	-0.0226
Higher Bound^	0.3823	0.3879	0.2823	0.3922	0.3882	0.2708
$\gamma_{tt}$	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	0.0007	0.0007	0.0004	0.0010	0.0011	0.0006
Median	0.0008	0.0007	0.0004	0.0010	0.0011	0.0006
Stdev	0.0029	0.0028	0.0022	0.0029	0.0028	0.0021
Lower Bound^	-0.0051	-0.0050	-0.0038	-0.0048	-0.0046	-0.0036
Higher Bound^	0.0063	0.0061	0.0048	0.0065	0.0065	0.0046
<b>Y</b>	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
γ <sub>tWk</sub> Mean	0.0066	0.0065	0.0041	0.0078	0.0074	0.0049
Median	0.0068	0.0066	0.0044	0.0077	0.0073	0.0050
Stdev	0.0051	0.0051	0.0047	0.0049	0.0047	0.0039
Lower Bound^	-0.0038	-0.0040	-0.0059	-0.0018	-0.0020	-0.0031
Higher Bound^	0.0162	0.0164	0.0125	0.0178	0.0167	0.0124
C						
¥	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
<b>Υ</b> twı Mean	-0.0445	-0.0434	-0.0491	-0.0538	-0.0547	-0.0559
Median	-0.0443	-0.0434	-0.0491	-0.0536	-0.0547	-0.0555
Stdev	0.0204	0.0203	0.0209	0.0174	0.0180	0.0175
Lower Bound^	-0.0834	-0.0203	-0.0203	-0.0883	-0.0907	-0.0891
Higher Bound^	-0.0034	-0.0023	-0.0078	-0.0385	-0.0307	-0.0207
ingrici bound	0.0042	0.00+0	0.0070	0.0100	0.0105	0.0207

Table 2. Parameter	estimates for Models 1	through 6 (continued).
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Table 2. Parame		0		e ,	<i>,</i>	
$\gamma_{tWm}$	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	-0.0139	-0.0127	-0.0221	-0.0166	-0.0169	-0.0198
Median	-0.0131	-0.0124	-0.0211	-0.0175	-0.0181	-0.0207
Stdev	0.0200	0.0194	0.0205	0.0138	0.0140	0.0136
Lower Bound^	-0.0559	-0.0532	-0.0646	-0.0412	-0.0411	-0.0443
Higher Bound^	0.0237	0.0237	0.0157	0.0125	0.0132	0.0087
$\gamma_{Wk}$	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	0.2215	0.2197	0.1526	0.2481	0.2392	0.1789
Median	0.2211	0.2213	0.1562	0.2452	0.2384	0.1798
Stdev	0.1663	0.1669	0.1595	0.1643	0.1605	0.1449
Lower Bound^	-0.1011	-0.1181	-0.1785	-0.0748	-0.0784	-0.1036
Higher Bound^	0.5465	0.5398	0.4506	0.5727	0.5448	0.4686
Υwı	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	3.8243	3.7841	3.6529	3.7145	3.7169	3.5287
Median	3.8260	3.7754	3.6574	3.7158	3.7240	3.5335
Stdev	0.8893	0.8587	0.8082	0.9252	0.9044	0.8417
Lower Bound^	2.1075	2.1082	2.0535	1.8379	1.9308	1.8595
Higher Bound^	5.5868	5.5185	5.2481	5.5724	5.4691	5.1659
$\gamma_{Wm}$	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	1.3104	1.3152	1.1005	1.2079	1.2113	1.1450
Median	1.3103	1.3092	1.1187	1.2050	1.2132	1.1290
Stdev	0.7739	0.7839	0.7711	0.7247	0.7137	0.6911
Lower Bound <sup>^</sup>	-0.2340	-0.2206	-0.4364	-0.1757	-0.1532	-0.1702
Higher Bound^	2.8484	2.8494	2.5658	2.6340	2.6655	2.5177
Υ <i>wkwk</i>	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	-0.5553	-0.5529	-0.5173	-0.5345	-0.5289	-0.4868
Median	-0.5546	-0.5554	-0.5222	-0.5343	-0.5324	-0.4891
Stdev	0.1196	0.1187	0.1130	0.1196	0.1213	0.1127
Lower Bound^	-0.7896	-0.7854	-0.7296	-0.7671	-0.7627	-0.6914
Higher Bound^	-0.3215	-0.3106	-0.2895	-0.2883	-0.2788	-0.2516
Υωιωι	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	-0.7962	-0.8025	-0.8111	-0.5736	-0.5765	-0.6362
Mean Median	-0.7962 -0.7874	-0.8025 -0.7967	-0.8111 -0.8061	-0.5736 -0.5647	-0.5765 -0.5746	-0.6362 -0.6292
Mean Median Stdev	-0.7962 -0.7874 0.3139	-0.8025 -0.7967 0.3122	-0.8111 -0.8061 0.3119	-0.5736 -0.5647 0.3197	-0.5765 -0.5746 0.3213	-0.6362 -0.6292 0.3155
Mean Median	-0.7962 -0.7874	-0.8025 -0.7967	-0.8111 -0.8061	-0.5736 -0.5647	-0.5765 -0.5746	-0.6362 -0.6292

# Table 2. Parameter estimates for Models 1 through 6 (continued).

Table 2. Paramet		0		0	,	
ŶWmWm	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	-0.7028	-0.7280	-0.6190	-0.6029	-0.6121	-0.6553
Median	-0.7170	-0.7296	-0.6260	-0.5800	-0.5845	-0.6290
Stdev	0.4546	0.4405	0.4632	0.3432	0.3426	0.3198
Lower Bound^	-1.5799	-1.5613	-1.4802	-1.3175	-1.3644	-1.3383
Higher Bound^	0.2503	0.1740	0.3522	-0.0307	-0.0342	-0.1272
Ŷwĸwi	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	-0.0839	-0.0843	-0.0886	-0.0729	-0.0726	-0.0807
Median	-0.0846	-0.0844	-0.0882	-0.0733	-0.0717	-0.0805
Stdev	0.0508	0.0506	0.0493	0.0474	0.0482	0.0447
Lower Bound <sup>^</sup>	-0.1881	-0.1851	-0.1846	-0.1666	-0.1707	-0.1669
Higher Bound^	0.0142	0.0138	0.0049	0.0174	0.0191	0.0063
<b>Y</b> WkWm	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	0.2148	0.2144	0.2523	0.1483	0.1554	0.1877
Median	0.2149	0.2129	0.2502	0.1497	0.1574	0.1900
Stdev	0.0972	0.0958	0.0879	0.0873	0.0859	0.0766
Lower Bound^	0.0223	0.0252	0.0831	-0.0206	-0.0096	0.0286
Higher Bound^	0.4003	0.4049	0.4296	0.3102	0.3207	0.3366
ŶwlWm	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	-0.1536	-0.1677	-0.1322	-0.0398	-0.0349	-0.0469
Median	-0.1560	-0.1689	-0.1387	-0.0162	-0.0114	-0.0285
Stdev	0.2554	0.2536	0.2614	0.1449	0.1507	0.1544
Lower Bound^	-0.6506	-0.6708	-0.6311	-0.3761	-0.3890	-0.3921
Higher Bound^	0.3606	0.3212	0.3898	0.2065	0.2275	0.2239
$\gamma_Y$	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	-0.6251	-0.6231	-0.3693	-0.6427	-0.6311	-0.3772
Median	-0.6228	-0.6296	-0.3827	-0.6494	-0.6252	-0.4032
Stdev	0.5701	0.5680	0.3605	0.5868	0.5651	0.3593
Lower Bound^	-1.7344	-1.7462	-1.0280	-1.8034	-1.7689	-1.0592
Higher Bound^	0.4542	0.4948	0.3765	0.5110	0.4595	0.3633
$\gamma_{YY}$	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	0.0460	0.0463	0.0254	0.0475	0.0468	0.0269
Median	0.0463	0.0465	0.0259	0.0478	0.0464	0.0286
Stdev	0.0462	0.0458	0.0293	0.0473	0.0455	0.0290
Lower Bound <sup>^</sup>	-0.0413	-0.0440	-0.0351	-0.0456	-0.0417	-0.0330
Higher Bound^	0.1343	0.1387	0.0786	0.1414	0.1397	0.0816

Table 2. Parameter	estimates fo	r Models 1	through 6	(continued).

ier commun			1811 0 (001		
Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
-0.0149	-0.0151	-0.0119	-0.0140	-0.0143	-0.0113
-0.0148	-0.0150	-0.0116	-0.0140	-0.0144	-0.0110
0.0092	0.0090	0.0061	0.0096	0.0091	0.0060
-0.0328	-0.0336	-0.0246	-0.0334	-0.0332	-0.0238
0.0039	0.0026	-0.0009	0.0050	0.0028	-0.0008
Model 1	Model 2	Model 3		Model 5	Model 6
0.0115	0.0118	0.0162	0.0096	0.0101	0.0148
0.0114	0.0116	0.0157	0.0096	0.0100	0.0147
	0.0096	0.0091			0.0087
-0.0068	-0.0068	-0.0007	-0.0090	-0.0078	-0.0019
0.0307	0.0313	0.0348	0.0286	0.0283	0.0321
					Model 6
					0.0214
					0.0202
					0.0493
					-0.0736
A 4000					0 1 1 1 0
0.1090	0.1059	0.1229	0.1086	0.1064	0.1220
Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Model 1 0.2167	Model 2 0.2157	Model 3 0.2534	Model 4 0.2085	Model 5 0.2103	Model 6 0.2379
Model 1 0.2167 0.2148	Model 2 0.2157 0.2134	Model 3 0.2534 0.2511	Model 4 0.2085 0.2067	Model 5 0.2103 0.2081	Model 6 0.2379 0.2374
Model 1 0.2167 0.2148 0.0589	Model 2 0.2157 0.2134 0.0577	Model 3 0.2534 0.2511 0.0551	Model 4 0.2085 0.2067 0.0535	Model 5 0.2103 0.2081 0.0537	Model 6 0.2379 0.2374 0.0522
Model 1 0.2167 0.2148 0.0589 0.1094	Model 2 0.2157 0.2134 0.0577 0.1076	Model 3 0.2534 0.2511 0.0551 0.1521	Model 4 0.2085 0.2067 0.0535 0.1076	Model 5 0.2103 0.2081 0.0537 0.1070	Model 6 0.2379 0.2374 0.0522 0.1393
Model 1 0.2167 0.2148 0.0589	Model 2 0.2157 0.2134 0.0577	Model 3 0.2534 0.2511 0.0551	Model 4 0.2085 0.2067 0.0535	Model 5 0.2103 0.2081 0.0537	Model 6 0.2379 0.2374 0.0522
Model 1 0.2167 0.2148 0.0589 0.1094 0.3396	Model 2 0.2157 0.2134 0.0577 0.1076	Model 3 0.2534 0.2511 0.0551 0.1521 0.3675	Model 4 0.2085 0.2067 0.0535 0.1076	Model 5 0.2103 0.2081 0.0537 0.1070	Model 6 0.2379 0.2374 0.0522 0.1393 0.3415
Model 1 0.2167 0.2148 0.0589 0.1094	Model 2 0.2157 0.2134 0.0577 0.1076 0.3319	Model 3 0.2534 0.2511 0.0551 0.1521	Model 4 0.2085 0.2067 0.0535 0.1076 0.3182	Model 5 0.2103 0.2081 0.0537 0.1070 0.3201	Model 6 0.2379 0.2374 0.0522 0.1393
Model 1 0.2167 0.2148 0.0589 0.1094 0.3396 Model 1	Model 2 0.2157 0.2134 0.0577 0.1076 0.3319 Model 2	Model 3 0.2534 0.2511 0.0551 0.1521 0.3675 Model 3	Model 4 0.2085 0.2067 0.0535 0.1076 0.3182 Model 4	Model 5 0.2103 0.2081 0.0537 0.1070 0.3201 Model 5	Model 6 0.2379 0.2374 0.0522 0.1393 0.3415 Model 6
Model 1 0.2167 0.2148 0.0589 0.1094 0.3396 Model 1 0.5146	Model 2 0.2157 0.2134 0.0577 0.1076 0.3319 Model 2 0.5175	Model 3 0.2534 0.2511 0.0551 0.1521 0.3675 Model 3 0.4831	Model 4 0.2085 0.2067 0.0535 0.1076 0.3182 Model 4 0.5334	Model 5 0.2103 0.2081 0.0537 0.1070 0.3201 Model 5 0.5314	Model 6 0.2379 0.2374 0.0522 0.1393 0.3415 Model 6 0.5006
Model 1 0.2167 0.2148 0.0589 0.1094 0.3396 Model 1 0.5146 0.5107	Model 2 0.2157 0.2134 0.0577 0.1076 0.3319 Model 2 0.5175 0.5148	Model 3 0.2534 0.2511 0.0551 0.1521 0.3675 Model 3 0.4831 0.4820	Model 4 0.2085 0.2067 0.0535 0.1076 0.3182 Model 4 0.5334 0.5298	Model 5 0.2103 0.2081 0.0537 0.1070 0.3201 Model 5 0.5314 0.5291	Model 6 0.2379 0.2374 0.0522 0.1393 0.3415 Model 6 0.5006 0.4969
Model 1 0.2167 0.2148 0.0589 0.1094 0.3396 Model 1 0.5146 0.5107 0.0764	Model 2 0.2157 0.2134 0.0577 0.1076 0.3319 Model 2 0.5175 0.5148 0.0775	Model 3 0.2534 0.2511 0.0551 0.1521 0.3675 Model 3 0.4831 0.4820 0.0675	Model 4 0.2085 0.2067 0.0535 0.1076 0.3182 Model 4 0.5334 0.5298 0.0794	Model 5 0.2103 0.2081 0.0537 0.1070 0.3201 Model 5 0.5314 0.5291 0.0782	Model 6 0.2379 0.2374 0.0522 0.1393 0.3415 Model 6 0.5006 0.4969 0.0713
Model 1 0.2167 0.2148 0.0589 0.1094 0.3396 Model 1 0.5146 0.5107 0.0764 0.3702	Model 2 0.2157 0.2134 0.0577 0.1076 0.3319 Model 2 0.5175 0.5148 0.0775 0.3707	Model 3 0.2534 0.2511 0.0551 0.1521 0.3675 Model 3 0.4831 0.4820 0.0675 0.3538	Model 4 0.2085 0.2067 0.0535 0.1076 0.3182 Model 4 0.5334 0.5298 0.0794 0.3882	Model 5 0.2103 0.2081 0.0537 0.1070 0.3201 Model 5 0.5314 0.5291 0.0782 0.3854	Model 6 0.2379 0.2374 0.0522 0.1393 0.3415 Model 6 0.5006 0.4969 0.0713 0.3672
Model 1 0.2167 0.2148 0.0589 0.1094 0.3396 Model 1 0.5146 0.5107 0.0764 0.3702	Model 2 0.2157 0.2134 0.0577 0.1076 0.3319 Model 2 0.5175 0.5148 0.0775 0.3707	Model 3 0.2534 0.2511 0.0551 0.1521 0.3675 Model 3 0.4831 0.4820 0.0675 0.3538	Model 4 0.2085 0.2067 0.0535 0.1076 0.3182 Model 4 0.5334 0.5298 0.0794 0.3882	Model 5 0.2103 0.2081 0.0537 0.1070 0.3201 Model 5 0.5314 0.5291 0.0782 0.3854	Model 6 0.2379 0.2374 0.0522 0.1393 0.3415 Model 6 0.5006 0.4969 0.0713 0.3672
Model 1 0.2167 0.2148 0.0589 0.1094 0.3396 Model 1 0.5146 0.5107 0.0764 0.3702 0.6734	Model 2 0.2157 0.2134 0.0577 0.1076 0.3319 Model 2 0.5175 0.5148 0.0775 0.3707 0.6773	Model 3 0.2534 0.2511 0.0551 0.1521 0.3675 Model 3 0.4831 0.4820 0.0675 0.3538 0.6146	Model 4 0.2085 0.2067 0.0535 0.1076 0.3182 Model 4 0.5334 0.5298 0.0794 0.3882 0.6984	Model 5 0.2103 0.2081 0.0537 0.1070 0.3201 Model 5 0.5314 0.5291 0.0782 0.3854 0.6879	Model 6 0.2379 0.2374 0.0522 0.1393 0.3415 Model 6 0.5006 0.4969 0.0713 0.3672 0.6442
Model 1 0.2167 0.2148 0.0589 0.1094 0.3396 Model 1 0.5146 0.5107 0.0764 0.3702 0.6734 Model 1	Model 2 0.2157 0.2134 0.0577 0.1076 0.3319 Model 2 0.5175 0.5148 0.0775 0.3707 0.6773	Model 3 0.2534 0.2511 0.0551 0.3675 Model 3 0.4831 0.4820 0.0675 0.3538 0.6146 Model 3	Model 4 0.2085 0.2067 0.0535 0.1076 0.3182 Model 4 0.5334 0.5298 0.0794 0.3882 0.6984 Model 4	Model 5 0.2103 0.2081 0.0537 0.1070 0.3201 Model 5 0.5314 0.5291 0.0782 0.3854 0.6879 Model 5	Model 6 0.2379 0.2374 0.0522 0.1393 0.3415 Model 6 0.5006 0.4969 0.0713 0.3672 0.6442 Model 6
Model 1 0.2167 0.2148 0.0589 0.1094 0.3396 Model 1 0.5146 0.5107 0.0764 0.3702 0.6734 Model 1 0.9273	Model 2 0.2157 0.2134 0.0577 0.1076 0.3319 Model 2 0.5175 0.5148 0.0775 0.3707 0.6773 Model 2 0.9263	Model 3 0.2534 0.2511 0.0551 0.1521 0.3675 Model 3 0.4831 0.4820 0.0675 0.3538 0.6146 Model 3 0.9079 0.9108 0.0253	Model 4 0.2085 0.2067 0.0535 0.1076 0.3182 Model 4 0.5334 0.5298 0.0794 0.3882 0.6984 Model 4 0.9432	Model 5 0.2103 0.2081 0.0537 0.1070 0.3201 Model 5 0.5314 0.5291 0.0782 0.3854 0.6879 Model 5 0.9399	Model 6 0.2379 0.2374 0.0522 0.1393 0.3415 Model 6 0.5006 0.4969 0.0713 0.3672 0.6442 Model 6 0.9185
Model 1 0.2167 0.2148 0.0589 0.1094 0.3396 Model 1 0.5146 0.5107 0.0764 0.3702 0.6734 Model 1 0.9273 0.9287	Model 2 0.2157 0.2134 0.0577 0.1076 0.3319 Model 2 0.5175 0.5148 0.0775 0.3707 0.6773 Model 2 0.9263 0.9271	Model 3 0.2534 0.2511 0.0551 0.3675 Model 3 0.4831 0.4820 0.0675 0.3538 0.6146 Model 3 0.9079 0.9108	Model 4 0.2085 0.2067 0.0535 0.1076 0.3182 Model 4 0.5334 0.5298 0.0794 0.3882 0.6984 Model 4 0.9432 0.9436	Model 5 0.2103 0.2081 0.0537 0.1070 0.3201 Model 5 0.5314 0.5291 0.0782 0.3854 0.6879 Model 5 0.9399 0.9409	Model 6 0.2379 0.2374 0.0522 0.1393 0.3415 Model 6 0.5006 0.4969 0.0713 0.3672 0.6442 Model 6 0.9185 0.9218
	Model 1 -0.0149 -0.0148 0.0092 -0.0328 0.0039 Model 1 0.0115 0.0114 0.0096 -0.0068 0.0307 Model 1 0.0050 0.0047 0.00517 -0.0989	Model 1 Model 2   -0.0149 -0.0151   -0.0148 -0.0150   0.0092 0.0090   -0.0328 -0.0336   0.0039 0.0026   Model 1 Model 2   0.0115 0.0118   0.0114 0.0116   0.0096 0.0096   -0.0068 -0.0068   0.0307 0.0313   Model 1 Model 2   0.0050 0.0063   0.0047 0.0063   0.0517 0.0502   -0.0989 -0.0913	Model 1   Model 2   Model 3     -0.0149   -0.0151   -0.0119     -0.0148   -0.0150   -0.0116     0.0092   0.0090   0.0061     -0.0328   -0.0336   -0.0246     0.0039   0.0026   -0.0009     Model 1   Model 2   Model 3     0.0115   0.0118   0.0162     0.0114   0.0116   0.0157     0.0096   0.0096   0.0091     -0.0068   -0.0068   -0.0007     0.0307   0.0313   0.0348     Model 1   Model 2   Model 3     0.0050   0.0063   0.0246     0.0047   0.0063   0.0242     0.0517   0.0502   0.0483     -0.0989   -0.0913   -0.0680	Model 1   Model 2   Model 3   Model 4     -0.0149   -0.0151   -0.0119   -0.0140     -0.0148   -0.0150   -0.0116   -0.0140     0.0092   0.0090   0.0061   0.0096     -0.0328   -0.0336   -0.0246   -0.0334     0.0039   0.0026   -0.0009   0.0050     Model 1   Model 2   Model 3   Model 4     0.0115   0.0118   0.0162   0.0096     0.0114   0.0116   0.0157   0.0096     0.0114   0.0116   0.0157   0.0096     0.0096   0.0096   0.0091   0.0095     -0.0068   -0.0068   -0.0007   -0.0090     0.0307   0.0313   0.0348   0.0286     Model 1   Model 2   Model 3   Model 4     0.0050   0.0063   0.0246   -0.0018     0.0047   0.0063   0.0242   -0.0018     0.0517   0.0502   0.0483   0.0530     -0.0989   -0.0913	-0.0149-0.0151-0.0119-0.0140-0.0143-0.0148-0.0150-0.0116-0.0140-0.01440.00920.00900.00610.00960.0091-0.0328-0.0336-0.0246-0.0334-0.03320.00390.0026-0.00090.00500.0028Model 1Model 2Model 3Model 4Model 50.01150.01180.01620.00960.01010.01440.01160.01570.00960.01020.00960.00960.00910.00950.0092-0.0068-0.0068-0.0007-0.0090-0.00780.03070.03130.03480.02860.0283Model 1Model 2Model 3Model 4Model 50.03070.03130.03480.02860.0283Model 1Model 2Model 3Model 4Model 50.03070.00630.0246-0.00660.00990.00470.0630.0242-0.00180.00020.05170.05020.04830.05300.0518-0.0989-0.0913-0.0680-0.1014-0.0996

#### Model 1 Model 2 Model 3 Model 4 Model 5 Model 6 $\alpha_L$ 0.3678 0.3431 0.3479 Mean 0.3604 0.3530 0.3419 Median 0.3586 0.3666 0.3420 0.3534 0.3490 0.3411 Stdev 0.1098 0.1073 0.1066 0.1063 0.1065 0.1032 Lower Bound^ 0.1482 0.1612 0.1349 0.1364 0.1415 0.1417 **Higher Bound^** 0.5775 0.5835 0.5520 0.5650 0.5556 0.5421 Model 6 Model 1 Model 2 Model 3 Model 4 Model 5 $\alpha_M$ 0.4432 0.3770 0.4493 Mean 0.4368 0.4533 0.4066 Median 0.4390 0.4444 0.3799 0.4556 0.4469 0.4052 0.1072 Stdev 0.1148 0.1136 0.1081 0.1075 0.1021 Lower Bound^ 0.2110 0.2225 0.1651 0.2441 0.2407 0.2120 **Higher Bound^** 0.6586 0.6638 0.6526 0.6626 0.5861 0.6078 Model 1 Model 2 Model 3 Model 4 Model 5 Model 6 $\sigma_{C}$ Mean 0.5019 0.5020 0.4955 0.5030 0.5022 0.5012 Median 0.4964 0.4959 0.4915 0.4977 0.4964 0.4978 0.0589 Stdev 0.0594 0.0556 0.0594 0.0581 0.0572 0.4048 Lower Bound^ 0.4022 0.4031 0.3992 0.4022 0.4034 **Higher Bound^** 0.6371 0.6174 0.6316 0.6298 0.6310 0.6241 Model 1 Model 2 Model 3 Model 4 Model 5 Model 6 $\sigma_K$ Mean 0.0549 0.0549 0.0557 0.0549 0.0551 0.0559 Median 0.0542 0.0540 0.0551 0.0541 0.0545 0.0550 Stdev 0.0071 0.0074 0.0074 0.0070 0.0073 0.0075 Lower Bound^ 0.0431 0.0429 0.0432 0.0431 0.0429 0.0440 **Higher Bound^** 0.0707 0.0719 0.0718 0.0707 0.0722 0.0734 Model 1 Model 2 Model 3 Model 4 Model 5 Model 6 $\sigma_L$ Mean 0.3769 0.3759 0.3790 0.3746 0.3747 0.3768 Median 0.3745 0.3715 0.3753 0.3712 0.3699 0.3718 Stdev 0.0437 0.0448 0.0445 0.0436 0.0448 0.0466 Lower Bound^ 0.3020 0.3008 0.3020 0.2997 0.2991 0.2999 **Higher Bound^** 0.4747 0.4738 0.4790 0.4677 0.4724 0.4825 Model 1 Model 2 Model 3 Model 4 Model 5 Model 6 $\sigma_M$ Mean 0.3341 0.3323 0.3470 0.3230 0.3234 0.3332 Median 0.3289 0.3282 0.3429 0.3187 0.3194 0.3291 Stdev 0.0462 0.0458 0.0462 0.0430 0.0421 0.0435 Lower Bound^ 0.2582 0.2556 0.2693 0.2516 0.2509 0.2578 **Higher Bound^** 0.4383 0.4362 0.4517 0.4197 0.4161 0.4257

#### Table 2. Parameter estimates for Models 1 through 6 (continued).

Table 2. Parameter estimates for Models 1 through 6 (cor	ntinued).
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Model 1	Model 2		Model 4	Model 5	Model 6
0.3201	0.3226	0.3634	0.3075	0.3112	0.3591
0.3257	0.3364	0.3716	0.3151	0.3168	0.3675
0.1476	0.1498	0.1387	0.1495	0.1474	0.1361
0.0178	0.0014	0.0663	-0.0113	0.0127	0.0665
0.5873	0.5902	0.6121	0.5698	0.5802	0.6074
Model 1	Model 2	Model 3	Model 4		Model 6
0.4551	0.4512	0.4563	0.4243	0.4251	0.4332
0.4644	0.4616	0.4674	0.4333	0.4364	0.4397
0.1301	0.1308	0.1288	0.1368	0.1354	0.1328
0.1734	0.1698	0.1798	0.1320	0.1314	0.1645
0.6815	0.6748	0.6821	0.6639	0.6664	0.6652
					Model 6
					0.6214
0.6050	0.6041	0.6537	0.5906	0.5947	0.6380
0.1302	0.1307	0.1118	0.1376	0.1386	0.1219
0 2000	0.2860	0.3894	0.2645	0.2590	0.3413
0.2906	0.2800	0.5054		0.2350	
0.2906	0.2800	0.8195	0.7925	0.7956	0.8095
0.8012	0.7959	0.8195	0.7925	0.7956	0.8095
0.8012 Model 1	0.7959 Model 2	0.8195 Model 3	0.7925 Model 4	0.7956 Model 5	0.8095 Model 6
0.8012 Model 1 -0.0605	0.7959 Model 2 -0.0601	0.8195 Model 3 -0.0638	0.7925 Model 4 -0.0475	0.7956 Model 5 -0.0532	0.8095 Model 6 -0.0518
0.8012 Model 1 -0.0605 -0.0625	0.7959 Model 2 -0.0601 -0.0601	0.8195 Model 3 -0.0638 -0.0650	0.7925 Model 4 -0.0475 -0.0471	0.7956 Model 5 -0.0532 -0.0549	0.8095 Model 6 -0.0518 -0.0526
0.8012 Model 1 -0.0605 -0.0625 0.1464	0.7959 Model 2 -0.0601 -0.0601 0.1415	0.8195 Model 3 -0.0638 -0.0650 0.1418	0.7925 Model 4 -0.0475 -0.0471 0.1457	0.7956 Model 5 -0.0532 -0.0549 0.1416	0.8095 Model 6 -0.0518 -0.0526 0.1429
0.8012 Model 1 -0.0605 -0.0625 0.1464 -0.3355	0.7959 Model 2 -0.0601 -0.0601	0.8195 Model 3 -0.0638 -0.0650	0.7925 Model 4 -0.0475 -0.0471	0.7956 Model 5 -0.0532 -0.0549	0.8095 Model 6 -0.0518 -0.0526
0.8012 Model 1 -0.0605 -0.0625 0.1464 -0.3355 0.2282	0.7959 Model 2 -0.0601 -0.0601 0.1415	0.8195 Model 3 -0.0638 -0.0650 0.1418	0.7925 Model 4 -0.0475 -0.0471 0.1457	0.7956 Model 5 -0.0532 -0.0549 0.1416	0.8095 Model 6 -0.0518 -0.0526 0.1429
0.8012 Model 1 -0.0605 -0.0625 0.1464 -0.3355	0.7959 Model 2 -0.0601 -0.0601 0.1415 -0.3320	0.8195 Model 3 -0.0638 -0.0650 0.1418 -0.3353	0.7925 Model 4 -0.0475 -0.0471 0.1457 -0.3273	0.7956 Model 5 -0.0532 -0.0549 0.1416 -0.3224	0.8095 Model 6 -0.0518 -0.0526 0.1429 -0.3331
0.8012 Model 1 -0.0605 -0.0625 0.1464 -0.3355 0.2282	0.7959 Model 2 -0.0601 -0.0601 0.1415 -0.3320 0.2270	0.8195 Model 3 -0.0638 -0.0650 0.1418 -0.3353 0.2086	0.7925 Model 4 -0.0475 -0.0471 0.1457 -0.3273 0.2364	0.7956 Model 5 -0.0532 -0.0549 0.1416 -0.3224 0.2271	0.8095 Model 6 -0.0518 -0.0526 0.1429 -0.3331 0.2315
0.8012 Model 1 -0.0605 -0.0625 0.1464 -0.3355 0.2282 Model 1	0.7959 Model 2 -0.0601 -0.0601 0.1415 -0.3320 0.2270 Model 2	0.8195 Model 3 -0.0638 -0.0650 0.1418 -0.3353 0.2086 Model 3	0.7925 Model 4 -0.0475 -0.0471 0.1457 -0.3273 0.2364 Model 4	0.7956 Model 5 -0.0532 -0.0549 0.1416 -0.3224 0.2271 Model 5	0.8095 Model 6 -0.0518 -0.0526 0.1429 -0.3331 0.2315 Model 6
0.8012 Model 1 -0.0605 -0.0625 0.1464 -0.3355 0.2282 Model 1 0.3028	0.7959 Model 2 -0.0601 -0.0601 0.1415 -0.3320 0.2270 Model 2 0.3086	0.8195 Model 3 -0.0638 -0.0650 0.1418 -0.3353 0.2086 Model 3 0.3956	0.7925 Model 4 -0.0475 -0.0471 0.1457 -0.3273 0.2364 Model 4 0.2705	0.7956 Model 5 -0.0532 -0.0549 0.1416 -0.3224 0.2271 Model 5 0.2811	0.8095 Model 6 -0.0518 -0.0526 0.1429 -0.3331 0.2315 Model 6 0.3781
0.8012 Model 1 -0.0605 -0.0625 0.1464 -0.3355 0.2282 Model 1 0.3028 0.3142	0.7959 Model 2 -0.0601 -0.0601 0.1415 -0.3320 0.2270 Model 2 0.3086 0.3172	0.8195 Model 3 -0.0638 -0.0650 0.1418 -0.3353 0.2086 Model 3 0.3956 0.4049	0.7925 Model 4 -0.0475 -0.0471 0.1457 -0.3273 0.2364 Model 4 0.2705 0.2780	0.7956 Model 5 -0.0532 -0.0549 0.1416 -0.3224 0.2271 Model 5 0.2811 0.2860	0.8095 Model 6 -0.0518 -0.0526 0.1429 -0.3331 0.2315 Model 6 0.3781 0.3851
0.8012 Model 1 -0.0605 -0.0625 0.1464 -0.3355 0.2282 Model 1 0.3028 0.3142 0.1946	0.7959 Model 2 -0.0601 -0.0601 0.1415 -0.3320 0.2270 Model 2 0.3086 0.3172 0.1875	0.8195 Model 3 -0.0638 -0.0650 0.1418 -0.3353 0.2086 Model 3 0.3956 0.4049 0.1668	0.7925 Model 4 -0.0475 -0.0471 0.1457 -0.3273 0.2364 Model 4 0.2705 0.2780 0.1896	0.7956 Model 5 -0.0532 -0.0549 0.1416 -0.3224 0.2271 Model 5 0.2811 0.2860 0.1819	0.8095 Model 6 -0.0518 -0.0526 0.1429 -0.3331 0.2315 Model 6 0.3781 0.3851 0.1590
0.8012 Model 1 -0.0605 -0.0625 0.1464 -0.3355 0.2282 Model 1 0.3028 0.3142 0.1946 -0.1070 0.6496	0.7959 Model 2 -0.0601 -0.0601 0.1415 -0.3320 0.2270 Model 2 0.3086 0.3172 0.1875 -0.0801 0.6454	0.8195 Model 3 -0.0638 -0.0650 0.1418 -0.3353 0.2086 Model 3 0.3956 0.4049 0.1668 0.0385 0.6864	0.7925 Model 4 -0.0475 -0.0471 0.1457 -0.3273 0.2364 Model 4 0.2705 0.2780 0.1896 -0.1193 0.6196	0.7956 Model 5 -0.0532 -0.0549 0.1416 -0.3224 0.2271 Model 5 0.2811 0.2860 0.1819 -0.0859 0.6099	0.8095 Model 6 -0.0518 -0.0526 0.1429 -0.3331 0.2315 Model 6 0.3781 0.3851 0.1590 0.0375 0.6634
0.8012 Model 1 -0.0605 -0.0625 0.1464 -0.3355 0.2282 Model 1 0.3028 0.3142 0.1946 -0.1070 0.6496 Model 1	0.7959 Model 2 -0.0601 -0.0601 0.1415 -0.3320 0.2270 Model 2 0.3086 0.3172 0.1875 -0.0801 0.6454	0.8195 Model 3 -0.0638 -0.0650 0.1418 -0.3353 0.2086 Model 3 0.3956 0.4049 0.1668 0.0385 0.6864 Model 3	0.7925 Model 4 -0.0475 -0.0471 0.1457 -0.3273 0.2364 Model 4 0.2705 0.2780 0.1896 -0.1193 0.6196	0.7956 Model 5 -0.0532 -0.0549 0.1416 -0.3224 0.2271 Model 5 0.2811 0.2860 0.1819 -0.0859 0.6099 Model 5	0.8095 Model 6 -0.0518 -0.0526 0.1429 -0.3331 0.2315 Model 6 0.3781 0.3851 0.1590 0.0375 0.6634 Model 6
0.8012 Model 1 -0.0605 -0.0625 0.1464 -0.3355 0.2282 Model 1 0.3028 0.3142 0.1946 -0.1070 0.6496 Model 1 0.2601	0.7959 Model 2 -0.0601 -0.0601 0.1415 -0.3320 0.2270 Model 2 0.3086 0.3172 0.1875 -0.0801 0.6454 Model 2 0.2626	0.8195 Model 3 -0.0638 -0.0650 0.1418 -0.3353 0.2086 Model 3 0.3956 0.4049 0.1668 0.0385 0.6864 Model 3 0.2369	0.7925 Model 4 -0.0475 -0.0471 0.1457 -0.3273 0.2364 Model 4 0.2705 0.2780 0.1896 -0.1193 0.6196 Model 4 0.2621	0.7956 Model 5 -0.0532 -0.0549 0.1416 -0.3224 0.2271 Model 5 0.2811 0.2860 0.1819 -0.0859 0.6099 Model 5 0.2535	0.8095 Model 6 -0.0518 -0.0526 0.1429 -0.3331 0.2315 Model 6 0.3781 0.3851 0.1590 0.0375 0.6634 Model 6 0.2478
0.8012 Model 1 -0.0605 -0.0625 0.1464 -0.3355 0.2282 Model 1 0.3028 0.3142 0.1946 -0.1070 0.6496 Model 1 0.2601 0.2690	0.7959 Model 2 -0.0601 -0.0601 0.1415 -0.3320 0.2270 Model 2 0.3086 0.3172 0.1875 -0.0801 0.6454 Model 2 0.2626 0.2663	0.8195 Model 3 -0.0638 -0.0650 0.1418 -0.3353 0.2086 Model 3 0.3956 0.4049 0.1668 0.0385 0.6864 Model 3 0.2369 0.2454	0.7925 Model 4 -0.0475 -0.0471 0.1457 -0.3273 0.2364 Model 4 0.2705 0.2780 0.1896 -0.1193 0.6196 Model 4 0.2621 0.2655	0.7956 Model 5 -0.0532 -0.0549 0.1416 -0.3224 0.2271 Model 5 0.2811 0.2860 0.1819 -0.0859 0.6099 Model 5 0.2535 0.2618	0.8095 Model 6 -0.0518 -0.0526 0.1429 -0.3331 0.2315 Model 6 0.3781 0.1590 0.0375 0.6634 Model 6 0.2478 0.2516
0.8012 Model 1 -0.0605 -0.0625 0.1464 -0.3355 0.2282 Model 1 0.3028 0.3142 0.1946 -0.1070 0.6496 Model 1 0.2601 0.2690 0.1410	0.7959 Model 2 -0.0601 -0.0601 0.1415 -0.3320 0.2270 Model 2 0.3086 0.3172 0.1875 -0.0801 0.6454 Model 2 0.2626 0.2663 0.1411	0.8195 Model 3 -0.0638 -0.0650 0.1418 -0.3353 0.2086 Model 3 0.3956 0.4049 0.1668 0.0385 0.6864 Model 3 0.2369 0.2454 0.1439	0.7925 Model 4 -0.0475 -0.0471 0.1457 -0.3273 0.2364 Model 4 0.2705 0.2780 0.1896 -0.1193 0.6196 Model 4 0.2621 0.2655 0.1364	0.7956 Model 5 -0.0532 -0.0549 0.1416 -0.3224 0.2271 Model 5 0.2811 0.2860 0.1819 -0.0859 0.6099 Model 5 0.2535 0.2618 0.1392	0.8095 Model 6 -0.0518 -0.0526 0.1429 -0.3331 0.2315 Model 6 0.3781 0.3851 0.1590 0.0375 0.6634 Model 6 0.2478 0.2516 0.1356
0.8012 Model 1 -0.0605 -0.0625 0.1464 -0.3355 0.2282 Model 1 0.3028 0.3142 0.1946 -0.1070 0.6496 Model 1 0.2601 0.2690	0.7959 Model 2 -0.0601 -0.0601 0.1415 -0.3320 0.2270 Model 2 0.3086 0.3172 0.1875 -0.0801 0.6454 Model 2 0.2626 0.2663	0.8195 Model 3 -0.0638 -0.0650 0.1418 -0.3353 0.2086 Model 3 0.3956 0.4049 0.1668 0.0385 0.6864 Model 3 0.2369 0.2454	0.7925 Model 4 -0.0475 -0.0471 0.1457 -0.3273 0.2364 Model 4 0.2705 0.2780 0.1896 -0.1193 0.6196 Model 4 0.2621 0.2655	0.7956 Model 5 -0.0532 -0.0549 0.1416 -0.3224 0.2271 Model 5 0.2811 0.2860 0.1819 -0.0859 0.6099 Model 5 0.2535 0.2618	0.8095 Model 6 -0.0518 -0.0526 0.1429 -0.3331 0.2315 Model 6 0.3781 0.1590 0.0375 0.6634 Model 6 0.2478 0.2516
	Model 1 0.3201 0.3257 0.1476 0.0178 0.5873 Model 1 0.4551 0.4644 0.1301 0.1734 0.6815 Model 1 0.5891 0.6050	Model 1   Model 2     0.3201   0.3226     0.3257   0.3364     0.1476   0.1498     0.0178   0.0014     0.5873   0.5902     Model 1   Model 2     0.4551   0.4512     0.4644   0.4616     0.1301   0.1308     0.1734   0.1698     0.6815   0.6748     Model 1   Model 2     0.5891   0.5893     0.6050   0.6041	Model 1   Model 2   Model 3     0.3201   0.3226   0.3634     0.3257   0.3364   0.3716     0.1476   0.1498   0.1387     0.0178   0.0014   0.0663     0.5873   0.5902   0.6121     Model 1   Model 2   Model 3     0.4551   0.4512   0.4563     0.4644   0.4616   0.4674     0.1301   0.1308   0.1288     0.1734   0.1698   0.1798     0.6815   0.6748   0.6821     Model 1   Model 2   Model 3     0.5891   0.5893   0.6383     0.6050   0.6041   0.6537	Model 1   Model 2   Model 3   Model 4     0.3201   0.3226   0.3634   0.3075     0.3257   0.3364   0.3716   0.3151     0.1476   0.1498   0.1387   0.1495     0.0178   0.0014   0.0663   -0.0113     0.5873   0.5902   0.6121   0.5698     Model 1   Model 2   Model 3   Model 4     0.4551   0.4512   0.4563   0.4243     0.4644   0.4616   0.4674   0.4333     0.1301   0.1308   0.1288   0.1368     0.1301   0.1308   0.1288   0.1368     0.1734   0.1698   0.1798   0.1320     0.6815   0.6748   0.6821   0.6639     Model 1   Model 2   Model 3   Model 4     0.5891   0.5893   0.6383   0.5728     0.6050   0.6041   0.6537   0.5906	0.32010.32260.36340.30750.31120.32570.33640.37160.31510.31680.14760.14980.13870.14950.14740.01780.00140.0663-0.01130.01270.58730.59020.61210.56980.5802Model 1Model 2Model 3Model 4Model 50.45510.45120.45630.42430.42510.46440.46160.46740.43330.43640.13010.13080.12880.13680.13540.17340.16980.17980.13200.13140.68150.67480.68210.66390.6664Model 1Model 2Model 3Model 4Model 50.58910.58930.63830.57280.57560.60500.60410.65370.59060.5947

Table 2.	Parameter	<sup>,</sup> estimates j	for	Models 1	through	6	(continued).

LikelihoodP	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	176.5424	176.6852	173.4191	173.7588	173.4520	166.5135
Median	176.8824	177.1389	173.8097	174.0793	173.9746	166.9548
Stdev	4.5932	4.9389	4.5839	4.9116	5.4077	4.9978
Lower Bound^	166.6852	165.7644	163.4715	163.1750	161.3069	156.0331
Higher Bound^	184.6299	184.8873	181.5127	182.2938	182.4634	174.9589

# Table 3. Cost elasticities for Models 1 through 6.

$\boldsymbol{\varepsilon}_{CY}$	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	0.240426	0.247187	0.28971	0.226974	0.233922	0.2826
Median	0.24264	0.246049	0.282801	0.228653	0.23174	0.275623
Stdev	0.108157	0.103564	0.089285	0.112803	0.10523	0.089941
Lower Bound^	0.022982	0.045575	0.133007	-0.00217	0.041418	0.125439
Higher Bound^	0.447214	0.454617	0.48358	0.439647	0.441744	0.471497

# Elasticity of Cost with respect to Output

# Semi-elasticity of Cost with respect to time

$\varepsilon_{Ct}$	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	-0.00741	-0.00736	-0.00837	-0.00758	-0.00773	-0.00827
Median	-0.00739	-0.0074	-0.00836	-0.00766	-0.00781	-0.00833
Stdev	0.002563	0.002576	0.002461	0.002389	0.00237	0.002219
Lower Bound^	-0.01241	-0.01226	-0.01314	-0.0121	-0.01209	-0.01236
Higher Bound^	-0.00236	-0.00227	-0.00355	-0.00273	-0.00298	-0.00383

# Table 4. Capital elasticities for Models 1 through 6.

Own-price elasticity

$\boldsymbol{\varepsilon}_{Kw_K}$	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	-0.15121	-0.15055	-0.14085	-0.14553	-0.14402	-0.13257
Median	-0.15102	-0.15122	-0.1422	-0.14549	-0.14497	-0.13318
Stdev	0.032576	0.032314	0.030766	0.032557	0.033019	0.030687
Lower Bound^	-0.215	-0.21385	-0.19868	-0.20887	-0.20768	-0.18825
Higher Bound^	-0.08754	-0.08457	-0.07882	-0.0785	-0.07592	-0.06851

# Elasticity of Capital with respect to Labor Price

$\varepsilon_{Kw_L}$	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	-0.01952	-0.0196	-0.02061	-0.01694	-0.01688	-0.01878
Median	-0.01968	-0.01963	-0.02052	-0.01706	-0.01667	-0.01873
Stdev	0.011824	0.011779	0.011476	0.011033	0.011201	0.010405
Lower Bound^	-0.04375	-0.04305	-0.04294	-0.03874	-0.0397	-0.03881
Higher Bound^	0.003313	0.003199	0.001139	0.004037	0.004435	0.001475

# Elasticity of Capital with respect to Price of Materials

$\varepsilon_{Kw_M}$	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	0.081603	0.081442	0.095852	0.056359	0.059044	0.07132
Median	0.081659	0.080879	0.095067	0.056881	0.059809	0.072191
Stdev	0.036924	0.036396	0.033389	0.033166	0.032649	0.029094
Lower Bound <sup>^</sup>	0.008471	0.009578	0.03158	-0.00781	-0.00364	0.010851
Higher Bound^	0.15208	0.153856	0.163234	0.117871	0.121836	0.12788

# Semi-Elasticity of Capital with respect to time

$\varepsilon_{Kt}$	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	0.002807	0.002781	0.001733	0.003301	0.003124	0.002076
Median	0.002884	0.002825	0.001876	0.003286	0.003121	0.002107
Stdev	0.002183	0.002165	0.00199	0.002095	0.002009	0.001662
Lower Bound^	-0.0016	-0.00169	-0.0025	-0.00077	-0.00085	-0.0013
Higher Bound^	0.006901	0.006952	0.005304	0.007573	0.007085	0.005281

# Table 5. Labor elasticities for Models 1 through 6.

#### Elasticity of Labor with respect to Capital Price

$\boldsymbol{\varepsilon}_{Lw_K}$	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	-0.01049	-0.01054	-0.01108	-0.00911	-0.00908	-0.01009
Median	-0.01058	-0.01055	-0.01103	-0.00917	-0.00896	-0.01007
Stdev	0.006356	0.006332	0.006169	0.005931	0.006021	0.005593
Lower Bound^	-0.02352	-0.02314	-0.02308	-0.02083	-0.02134	-0.02086
Higher Bound^	0.001781	0.001719	0.000612	0.00217	0.002384	0.000793

# Own-price elasticity

$arepsilon_{Lw_L}$	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	-0.08501	-0.08569	-0.0866	-0.06124	-0.06155	-0.06792
Median	-0.08407	-0.08507	-0.08607	-0.06029	-0.06135	-0.06718
Stdev	0.033515	0.033339	0.033304	0.034133	0.034311	0.033682
Lower Bound <sup>^</sup>	-0.1535	-0.15024	-0.15155	-0.13078	-0.12917	-0.13584
Higher Bound^	-0.0197	-0.02026	-0.02174	-0.00303	-0.0011	-0.00754

# Elasticity of Labor with respect to Price of Materials

$\varepsilon_{Lw_M}$	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	-0.02679	-0.02925	-0.02306	-0.00695	-0.0061	-0.00818
Median	-0.02721	-0.02947	-0.02419	-0.00283	-0.002	-0.00497
Stdev	0.044552	0.044233	0.045597	0.025271	0.02629	0.026933
Lower Bound <sup>^</sup>	-0.11349	-0.11701	-0.11008	-0.06561	-0.06786	-0.06839
Higher Bound^	0.062893	0.056023	0.067988	0.036025	0.039682	0.039057

# Semi-Elasticity of Labor with respect to time

$\varepsilon_{Lt}$	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	-0.00868	-0.00846	-0.00959	-0.01049	-0.01067	-0.01089
Median	-0.00872	-0.00844	-0.00955	-0.01045	-0.01073	-0.01104
Stdev	0.003987	0.003961	0.004076	0.003396	0.003507	0.003416
Lower Bound <sup>^</sup>	-0.01627	-0.01605	-0.01786	-0.01723	-0.01769	-0.01738
Higher Bound^	-0.00081	-0.00078	-0.00153	-0.00383	-0.00361	-0.00404

# Table 6. Materials elasticities for Models 1 through 6.

Elasticity of Materials with respect to Capital Price

$\mathcal{E}_{MWK}$	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	0.021937	0.021894	0.025768	0.015151	0.015873	0.019173
Median	0.021952	0.021743	0.025557	0.015291	0.016079	0.019407
Stdev	0.009926	0.009784	0.008976	0.008916	0.008777	0.007821
Lower Bound <sup>^</sup>	0.002277	0.002575	0.00849	-0.0021	-0.00098	0.002917
Higher Bound^	0.040884	0.041361	0.043882	0.031687	0.032753	0.034378

#### Elasticity of Materials with respect to Price of Capital

$\varepsilon_{Mw_L}$	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	-0.0134	-0.01463	-0.01153	-0.00348	-0.00305	-0.00409
Median	-0.01361	-0.01474	-0.0121	-0.00142	-0.001	-0.00248
Stdev	0.022281	0.022121	0.022803	0.012638	0.013147	0.013469
Lower Bound <sup>^</sup>	-0.05675	-0.05852	-0.05505	-0.03281	-0.03394	-0.0342
Higher Bound^	0.031453	0.028017	0.034001	0.018016	0.019845	0.019533

# Own-price elasticity

$\boldsymbol{\varepsilon}_{Mw_M}$	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	-0.10016	-0.10375	-0.08822	-0.08592	-0.08723	-0.0934
Median	-0.10219	-0.10399	-0.08922	-0.08266	-0.08331	-0.08964
Stdev	0.064788	0.062778	0.06602	0.048908	0.048829	0.045573
Lower Bound <sup>^</sup>	-0.22517	-0.22252	-0.21095	-0.18777	-0.19446	-0.19074
Higher Bound^	0.035672	0.024801	0.050189	-0.00437	-0.00488	-0.01813

# Semi-Elasticity of Materials with respect to time

$\varepsilon_{Mt}$	Model 1	Model 2	Model 3	Model 4	Model 5	Model 6
Mean	-0.00222	-0.00202	-0.00352	-0.00264	-0.0027	-0.00315
Median	-0.00209	-0.00197	-0.00337	-0.00279	-0.00288	-0.0033
Stdev	0.003193	0.003093	0.00327	0.0022	0.002227	0.002163
Lower Bound^	-0.00891	-0.00848	-0.01029	-0.00657	-0.00656	-0.00706
Higher Bound^	0.00377	0.003775	0.0025	0.001999	0.002103	0.00139